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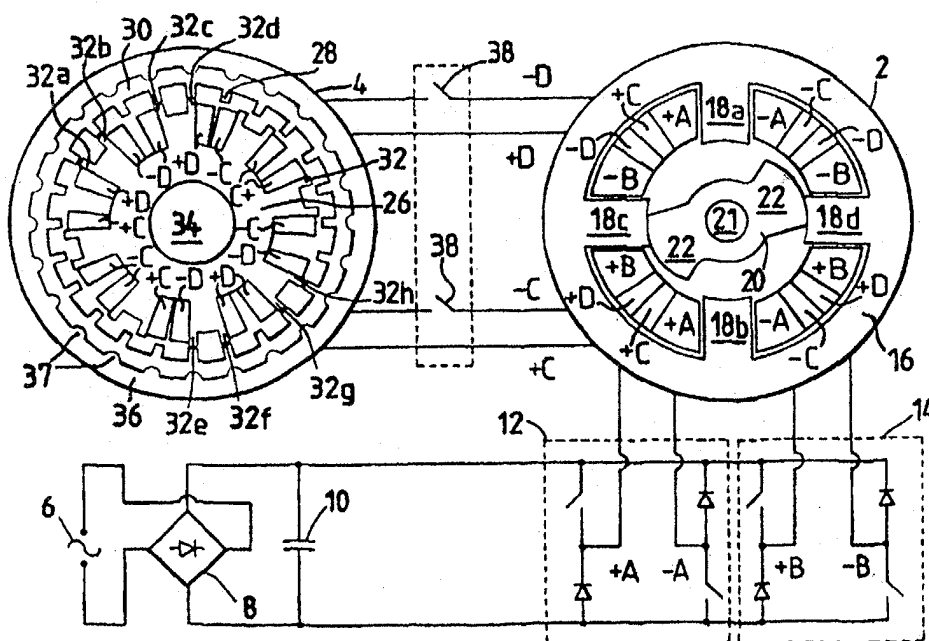
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(54) Title: A MOTOR



(57) Abstract

A motor comprising two or more rotors (20, 30) rotated by means of a common power supply (6), each rotor (20, 30) having a plurality of poles (22, 32) and being associated with a stator (16, 26) having a plurality of poles (18, 28), wherein the arrangement of rotor

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A MOTOR

The invention relates to a motor.

Many developments have been made over the years to motors, in particular to those motors which are used in domestic household appliances. However, it is generally believed that the trend of improvements in relation to universal motors is nearing its end. It is therefore an object of the present invention to provide a motor which is suitable for providing the appropriate power to various parts of a domestic household appliance and which also has scope for improvement beyond the potential of known universal motors.

Domestic household appliances such as vacuum cleaners very often include a universal motor adapted to drive the fan used to create the suction by means of which air is drawn into the vacuum cleaner. When the vacuum cleaner is an upright cleaner, a brush bar is usually mounted rotatably in the dirty air inlet located in the cleaner head. The brush bar is rotated by means of a drive belt extending between the motor and the brush bar. There are many disadvantages of this arrangement, not least of which is the vulnerability of the drive belt itself. Other disadvantages include the fact that, in most cases, the drive belt engages with a portion of the outer surface of the brush bar which means that brush bristles cannot be located in that area. It is also advantageous to have some sort of mechanism for preventing the brush bar from rotating against a carpet to be cleaned if, for any reason, the motor is left running whilst the vacuum cleaner remains stationary, for example, whilst carrying out above-floor cleaning.

In a cylinder cleaner, the dirty air inlet is situated at the end of a hose, hence a drive belt to the main vacuum motor is impractical, and driving the brush bar directly by a secondary universal motor has practical difficulties. Pneumatically powered "turbo" brushes have been proposed, but they are normally inefficient and reduce the power watts available for the pickup of dirt and dust by the cleaner head.

It is therefore an object of the invention to provide a vacuum cleaner having a driven brush bar but which reduces or eliminates the problems identified above.

According to the invention, a motor is provided in accordance with the features of claim 1. Preferred features of the invention are set out in the subsidiary claims.

The provision of at least two rotors in the motor has been identified as an economical and compact way of driving two separate features of a household appliance such as a vacuum cleaner at different speeds. Making use of the same winding or windings or a common power supply to drive two separate rotors is clearly advantageous in an environment in which consumers demand small, lightweight appliances.

A number of alternative embodiments of the invention will now be described by way of example with reference to the accompanying drawings in which:

Figure 1 is a schematic view of a primary and secondary motor arrangement which embodies the invention;

Figures 2a-2d are sectional and cross-sectional views of the brush bar incorporating the secondary motor of Figure 1;

Figures 3a-3d are sectional and cross-sectional views of a second brush bar incorporating a secondary motor such as shown in Figure 1;

Figures 4a-4i show portions of electrical circuits suitable for powering a secondary two-phase switched reluctance motor from a primary two-phase switched reluctance motor in accordance with the invention;

Figures 5a-5K show electrical circuit portions for use in powering a secondary single phase switched reluctance motor from a primary single phase switched reluctance motor in accordance with the invention;

Figures 6a-6s show a series of circuit portions which can be combined together for powering a secondary motor from a two-phase switched reluctance motor in accordance with the invention;

Figures 7a-7g are schematic cross-sectional views of various alternative motors in accordance with the present invention;

Figures 8a and 8b are schematic cross-sectional views of alternative motor arrangements in accordance with the invention;

Figure 9 is a schematic cross-sectional view of a motor in accordance with the present invention; and

Figure 10 is a still further cross-sectional view of a motor in accordance with the present invention.

Figure 1 shows a primary 4/2 two-phase switched reluctance motor 2, a secondary 24/16 two-phase switched reluctance motor 4 and a power supply circuit which is connected to the primary motor 2. Other types of switched reluctance motor, (e.g. single phase, three phase, four phase, etc) could be used for either motor, if desired. The arrangement shown is perceived as being particularly suitable for driving the fan and brush bar of a vacuum cleaner, although this is by no means the only application envisaged.

In common with known switched reluctance motors, the primary motor 2 comprises a stator 16 with four salient poles 18a-18d. Opposed poles 18a and 18b each support a like armature winding +A,-A which form a first phase. Opposed poles 18c and 18d accommodate respective like armature windings +B,-B which represent a second phase. A rotor 20 is rotatably mounted upon an axis 21 within the stator 16 and comprises opposed poles 22. The rotor 20 is formed from steel laminated in the axial direction.

Power is supplied to the motor 2 from a mains supply 6 which is rectified by a bridge rectifier 8. A capacitor 10 is provided for smoothing the bridge output. Each of the armature winding pairings A,B is fed via a respective asymmetric half bridge 12,14. Each half bridge 12,14 relates to a respective one of the two phases. In this regard, half bridge 12 supplies the A windings and half bridge 14 supplies the B windings.

For continuous operation, current is applied to each of the stator phases in turn at a rate which is dependent on and determined by the variation of the rotor position with time. The timing of the asymmetric half bridges 12,14 is determined by reference to the rotor positions of the primary and/or secondary motors by means of either optical or Hall effect sensors or any other suitable means.

The primary reluctance motor 2 also includes two additional winding pairs: C and D. One winding of winding pair C is accommodated on each of salient poles 18a and 18b. One winding of the winding pair D is accommodated on each of the salient poles 18c and 18d.

The respective pairings of windings A and C on the one hand and B and D on the other each operate in the manner of a transformer. The current induced in winding

+

pairs C and D by winding pairs A and B is supplied to the secondary reluctance motor 4. For convenience of assembly within the brush bar of the vacuum cleaner, this motor is structurally the inverse of the primary motor 2. That is to say, the rotor 30 is situated radially outside the stator 26, which is located upon a fixed axis 34. The radially inner surface of the brush bar 36 is fitted directly upon the radially outer surface of the rotor 30 and secured in place by splines 37.

Closer reference to Figure 1 will reveal that the stator 26 comprises sixteen poles 32. The rotor 30 comprises twenty-four radially inwardly directed poles 28. The poles 32 situated upon the stator 26 are arranged in pairs, with each pair being surrounded by a respective winding. The windings themselves are paired circumferentially and then these pairs of windings are in turn paired with a similar pair of windings situated on the radially opposite side of the stator. For example, poles 32a and 32b are provided with a D winding. Circumferentially adjacent poles 32c and 32d are provided with a second D winding. Radially opposite, poles 32e-32h are arranged in a similar fashion. The spacing between the poles 32a-32h is such as to enable their simultaneous radial correspondence with rotor poles 28, as shown in the figure. However, the poles associated with the D windings are radially off-set from the coils associated with the C windings, such that radial correspondence with the rotor poles cannot be achieved by the poles associated with the C coils at the same time as the poles associated with the D coils. Hence a two-phase structure results.

The number of poles provided in the secondary switched reluctance motor 2 ensures smooth rotation of the brush bar 36.

The power supply to the primary reluctance motor 4 is typically switched at a frequency of the order of 1.25 kHz per phase, (if a 4/4 single phase switched reluctance motor were used as the primary a switching frequency of about 2.5 kHz would be comparable). The secondary reluctance motor can be switched at the same, high frequency (or reduced ratio by disconnecting the secondary windings from the number of poles). As a consequence of this magnitude of frequency, there is no need to provide for a high level of flux build-up in the coil armature of the primary motor (or an intermediate transformer, if the voltage is stepped down outside the primary motor). Because the voltage to the secondary motor 4 is stepped-down and isolated from the voltage of the primary motor 2, the supply of power to the secondary motor is very safe.

In fact, the supply is so safe that the power can be fed via the hose to the suction head of a cylinder vacuum cleaner without a risk of compromising safety.

Supplying power to the primary motor 2 via the power supply circuit causes the primary rotor 22 to rotate within the stator 16. The current flowing within the coils A,B induces current in coils C,D which in turn causes the secondary rotor 30 to rotate about the secondary stator 36. The number of poles present on each stator 16,36 and rotor 22,30 determines the relative speeds of rotation; in this example, the secondary rotor 30 will rotate at one twelfth of the speed of the primary rotor 22.

Switches 38 are provided in order to enable the electrical connection to the windings C,D to be interrupted. The switches can be operated manually or triggered automatically in response to the conditions of the device in which the motor is situated. For example, it may be desirable to switch off the brush bar of a vacuum cleaner under some circumstances and operation of the switches 38 can achieve this. The switches can be made to open in the event that the handle of the vacuum cleaner is put into the upright position by means of simple electronic circuitry which will be readily available to a skilled reader. The switches can also be operated intermittently, for example during start-up of the brush bar, so that the rotation of the brush bar can be brought up to speed in a controlled and reliable manner.

By using a switched reluctance motor as the secondary motor 4, significant advantages arise. Due to the lack of commutating brushes, no carbon powder is generated by brush wear. Furthermore, the motor has a relatively long life and its speed is not limited by the need to maintain a reasonable brush life. Use of a switched reluctance motor as the primary motor enables a switched reluctance motor to be used as the secondary motor with relative ease.

Figures 2a-2d show the secondary motor 2 of Figure 1, situated within a vacuum cleaner brush bar 36, in more detail. Figure 2a is a section. Views 2b-2d are cross-sections taken along lines I to III in Figure 2a, respectively. Referring to Figure 2a, it will be seen that the brush bar 36 and rotor 28 are together mounted by means of bearings 40 upon the shaft 34 that supports the stator 26. The shaft 34 is mounted at each end to a housing 42 of the vacuum cleaner. From cross sectional Figure 2c, it will be seen that the shaft 34 includes four axial grooves 42 situated at circumferential

intervals (eg 90°). Each groove 42 accommodates a wire for supplying current from the primary motor 2 to the secondary motor 4.

Figures 3a-3d show a variation of the arrangement of Figure 2. Figure 3a is a section and Figures 3b to 3d are cross-sections taken along lines I to III in Figure 3a, respectively. In this embodiment, the shaft 34 is hollow and the wires for supplying current to the windings of the secondary motor run inside the shaft, as can clearly be seen from cross sectional Figure 3c.

Although the above embodiments have a greater number of poles in the secondary motor than in the primary motor, this is not necessary. The primary motor can have an equal or greater number of poles relative to the secondary motor if circumstances require it. For example on a washing machine, a primary motor used as a direct drive could operate at about 0-2000 rpm and drive a secondary motor for a high-speed water pump operating at 0-10,000 rpm. In such a case, it would be appropriate for the primary motor to have a greater number of poles than the secondary motor. In the case of the example mentioned, the primary motor will have a pole arrangement capable of driving the secondary motor at five times the speed of the primary motor.

Figure 4 shows some alternative circuit arrangements for supplying power from the primary two-phase switched reluctance motor 2 to the secondary switched reluctance motor 4 of Figure 1.

In each case, the first stage of the power supply circuit is the same as in Figure 1, that is to say it comprises an AC mains supply, a bridge rectifier and a smoothing capacitor. The circuits also each include a half bridge 12, 14 for supplying each respective phase winding of the primary motor as before. However, the connections for supplying the secondary motor are different in each case.

Figures 4g and 4i correspond generally to the arrangement of Figure 1. That is to say a pair of additional windings are provided on the primary motor which are connected directly to windings provided on the secondary motor. Figure 4i corresponds exactly to the arrangement of Figure 1: Figure 4g shows the same arrangement without the switches 38. Figure 4h shows a similar arrangement in which the motors are electrically connected in parallel and switches are also provided.

In Figure 4a, each of the windings on the secondary motor is connected in parallel with a respective one of the windings on the primary motor. Whilst this

arrangement is relatively simple, it does not isolate the windings on the secondary motor from those on the primary motor or provide for a voltage drop from the primary motor to the secondary motor.

Figure 4b shows a circuit in which each of the windings on the secondary motor is connected in series with a respective one of the windings on the primary motor. This provides a voltage drop from the primary motor to the secondary motor. However, once again, this does not provide for isolation of the secondary windings from the primary windings.

Figure 4c shows a circuit in which each of the secondary motor windings is tapped from a respective winding of the primary motor. This arrangement enables a selectable ratio of voltage drop between the primary motor and the secondary motor to be effected. However, the two motors are not electrically isolated.

Figures 4d-4f correspond with Figures 4a-4c, except that, in each case, a transformer is introduced between each secondary motor winding and its associated primary motor winding. This arrangement has the advantage of isolating the secondary motor windings from the primary motor windings and enabling the voltage to be stepped down between the primary motor windings and the secondary motor windings. By using switched reluctance motors operating at relatively high frequencies, such as 1.5 kHz per phase, flux build-up within the transformer will be relatively small and, therefore, a relatively compact, lightweight unit can be used which provides significant cost-savings and enables the overall weight of the appliance to be kept low.

Figure 5 relates to an appliance in which both the primary motor 2 and the secondary motor 4 are single-phase motors. Reference to Figures 5a-5h will show that circuits corresponding to those of Figure 4 may just as easily be employed in a single-phase arrangement as in a two-phase arrangement. Figures 5i and 5j correspond with Figure 5d, but incorporate an additional switch between the primary motor winding and the secondary motor winding, the switch being on an opposite side of the intermediate transformer in each respective case. Figure 5k corresponds with Figure 5g but, like Figures 5i and 5j, incorporates a switch between the primary motor winding and the secondary motor winding. These additional switches enable the frequency of operation of the secondary switched reluctance motor to be varied from the frequency of operation of the primary switched reluctance motor. The switches hence enable the secondary

motor to be re-started, if it stalls, by switching the applied current and thereby allowing sufficient inertia to build up in the rotor. The additional switches can be used to electrically interconnect the windings in sequence with primary switching poles so as to vary the secondary frequencies. The ratings of the switches can be minimised if desired by operating them under zero current switching conditions. In addition, the switches enable the supply to the secondary motor to be cut off, for safety, whilst cleaning with the vacuum cleaner hose/wand or cleaning the brush bar.

Figure 6 shows some further variations for powering a secondary motor from a primary two-phase switched reluctance motor.

Figure 6a is identical to the first stage of the power supply shown in Figure 1, that is to say it comprises an AC source coupled with a bridge rectifier and a smoothing capacitor. Figure 6b differs from Figure 6a only in that the smoothing capacitor has been omitted. Although this results in a consequent degradation in the DC waveform, benefits include significant cost and size savings and a potential increase in long-term reliability since there is no electrolyte which can detrimentally dry-out.

Figures 6c-6f correspond exactly with Figures 4d-4g, as does Figure 6g.

Figures 6h and 6i show parallel and series connection of the intermediate transformers, respectively. Figure 6j shows a common secondary winding in the intermediate transformer. The arrangements in Figures 6h-6j enable the output from both phases of a two-phase switched reluctance motor to be fed to a single-phase secondary switched reluctance motor.

As shown in Figure 6l, a switch may be connected to the output of Figures 6g-6j for motor speed control. Figure 6m shows rectified connections for powering a pair of DC motors. These motors may be smoothed, as shown in Figure 6q, or not, as in Figure 6r. Figures 6n and 6o show rectified parallel and series connections, respectively, for supplying a single DC motor. Of course, an AC motor, as shown in Figure 6s, may be employed using the direct connections of Figure 6p.

As will be apparent from Figure 6, the secondary motor need not be a switched reluctance motor.

Figure 7 illustrates various embodiments of the invention, in each of which one or more windings are used to drive more than one rotor of a single motor. Figure 7a illustrates an embodiment similar to those illustrated in Figures 1 to 3. The motor 500

has a stator 502 carrying a winding A and twenty four external poles 504. Rotatably mounted radially outwardly of the stator 502 is an external rotor 506, also carrying twenty four poles 508. A plurality of splines 510 are arranged between the external rotor 506 and the interior surface of a brush bar cylinder 512 of a vacuum cleaner. This arrangement can be used to cause rotation of the brush bar 512 in the same way as is described in relation to the earlier figures.

The main difference between the motor illustrated in Figure 7a and the previously illustrated motors is the provision of four internal poles 514 on the stator 502. Radially inwardly of the stator 502 is mounted a second, inner rotor 516 having four equispaced poles 518. The inner rotor 516 is rotatably mounted about a central axle 520.

It will be appreciated that, simultaneously with the rotation of the external rotor 506 when power is supplied to the winding A, the inner rotor 516 will also rotate. However, the speed of rotation of the inner rotor 516 will be six times the speed of rotation of the external rotor 526 due to the difference in the number poles provided on each rotor and the associated stator.

It will also be appreciated that this principle can be applied to many alternative arrangements and very many alternative variations are possible. Figures 7b, c, d, e and f each show, schematically, different arrangements of a single switched reluctance motor having a common winding or set of windings driving two separate rotors. In each case, the number of poles carried by each rotor is different. It will be appreciated that the number of poles on each rotor can be varied at will. Figure 7g illustrates schematically a two phase switched reluctance motor having two windings instead of one and also driving two separate rotors. One advantage of driving two separate rotors by means of one winding or set of windings is that the volume occupied by the motor will be reduced and the associated mass will therefore also be reduced.

The rotors of a motor in accordance with the invention can either rotate uni-, contra- or multi-directionally.

In the case of a switched reluctance motor, the initial direction of rotation is usually determined by the initial position of the rotor pole(s) relative to the stator pole(s) and/or the phase switching sequence(s) when a current pulse is applied to the winding(s).

If one considers the motors shown in Figure 7, it is possible to obtain either uni- or contra-directional rotation by locating the rotors at suitable respective orientations relative to the stator prior to the application of a current pulse. Figures 8a and 8b show a motor in which magnets 550 are provided for parking the rotors when the driving current is terminated, so that the rotors will be in a suitable position for contra-directional rotation when a current is next applied. In this regard, Figure 8a shows a motor with different speed outputs at an initial parking position prior to the application of a driving current. Figure 8b shows the direction of rotation of the respective rotors after the winding is excited. It will be seen from the figure that the two rotors rotate in respectively opposite directions. It will be seen that the magnets are strategically positioned in order to align each of the poles of the rotors to be closer to one particular pole than an adjacent pole. Therefore, when the coil is excited, each rotor pole moves towards that closest stator pole, thereby determining the direction of rotation. Naturally, a mechanism could be provided for adjusting the position of the magnets, so as to change the direction of rotation of a particular motor.

An alternative for multi-phase switched reluctance motors having more than one rotor is to arrange the phase sequences to be such that they produce either uni- or contra-directional rotation in the rotors. It is also possible to control the direction of the rotation by providing asymmetrical air gaps between the rotor and stator poles.

The above motor arrangements allow contra-directional rotating elements to be provided without a prohibitive increase in cost or mechanical complexity. The motor arrangements can also provide significant additional advantages as follows. First, net angular momentum can be cancelled or reduced. This leads to the minimization of acceleration/retardation reaction torques on both the motor and/or the appliance or product to which it is fitted. Furthermore, net gyroscopic effects can be cancelled or reduced. This leads to a minimisation of gyroscopic forces on the motor and/or the appliance or product when subject to general movement. Such motor arrangements also enable a reduction of acoustic and mechanical vibrations through various methods including superposition cancellation.

A motor having contra-directional rotors, such as described above, can provide significant advantages when used in a vacuum cleaner for rotating motorised dual or multiple cyclones. More specifically, the motor can be used to drive the impellers

inside the inner and outer bins directly. Further, if desired, the air flows through the inner and outer cyclones can be connected in series - resulting in a potential load matching between the motor's outputs and thus a simplification and reduction of the power electronics and/or mechanical complexity.

In the case of switched reluctance motors, the switching times of primary and/or additional windings can be controlled using information from position sensor(s) on the primary and/or additional rotor(s). If desired, the positional information of the rotors can be combined (e.g. via a microprocessor, combinational logic or physical construction of the sensor(s)) to give the desired operating characteristics for the motor and/or the product/appliance they are used within or in combination with. This allows for a potential simplification of the power electronics circuitry and thus a potential reduction in the overall cost, size and weight of the product/appliance.

Figures 9 and 10 show variations of the winding structure for a dual output single phase motor, such as shown in Figure 7a, for example. In each of Figures 9 and 10, the stator 502 is provided with two sets of windings. In this regard, a first winding 550 is wound around the radially inwardly directed poles 518 and a second winding 560 is wound around the radially outwardly directed poles 504.

Figure 10 shows a broadly similar arrangement, however there is some radial overlap between the radially inner windings 550 and the radially outer windings 560. This arrangement enables significant reductions in size for a given number of winding turns.

In vacuum cleaner applications, it is possible to provide more than one impeller to draw the air through the cleaner. Typically, and in accordance with the embodiment shown in Figure 11, a first impeller 570 can be arranged upstream of the bag (not shown) which separates the dirt and dust from the airflow whilst a second impeller 572 can be arranged downstream thereof. The first impeller 570 can be rotated more slowly than the second impeller 572 but can have a larger size to accommodate the passage of larger dust particles. The second impeller 572 can be made relatively smaller because it only sees finer dust particles. This facilitates an elevated operating speed which further improves the performance of the vacuum cleaner. Further, the ratio of the speeds of the rotors can be configured to compensate for the ratios of fan/rotor inertias thus allowing

for reduced or net zero gyroscopic forces. A third motor output could be provided to rotate a brush bar.

Looking at Figure 11 in more detail, the motor arrangement comprises a central mechanical support 574 supporting an axially central stator 576 provided with laminated poles 590. The poles 590 are provided with windings 578. A pair of axially aligned rotors 580, 581 are provided on respective axial sides of the stator 576. The impellers 570, 572 are provided on the axial sides of the rotors 580, 581 remote from the support 574. The impellers 570, 572 and rotors 580, 581 are mounted upon a central shaft 582 which is integrally formed with the support 574. Parking magnets 584 are provided for locating the poles 586 of each rotor 580, 581 closer to poles which are respectively on circumferentially opposite sides of the mid-point between any given adjacent pairing of stator poles 590. This has the effect of causing the rotors 580, 581 to rotate in opposite directions when the windings 578 are excited. To ensure that the impellers 570, 572 draw air from opposite sides of the motor arrangement, each impeller 570, 572 has vanes 588 which are oriented in the opposite direction to those of the other impeller. Air can thus be drawn from the dirty air inlet of the vacuum cleaner by the impeller 570, expelled from there to the dirt and dust collecting bag in which the air is cleaned, and then drawn back from the bag to the clean air outlet by the impeller 572.

Another application of the invention is the variation of the ratio of the speeds of a motor and a generator. An example of this type of application is the variation of the speeds of the turbine and the compressor in the turbo-charger on an internal combustion engine in an automotive vehicle as illustrated in Figure 12. This can be achieved in practice by the use of a switched reluctance motor 610 to drive the compressor 612 and a switched reluctance generator 614 to absorb the energy of the turbine 616. The speed of the compressor 612 can be synchronised to an integer multiple of the speed of the turbine 616 and to the combination of the ratios of the motor/generator poles so that the input power per "stroke" of the generator 614 can be transferred directly to the output power per "stroke" of the motor 610. Such a variable ratio turbo-charger has many advantages over a standard unity ratio turbo-charger, including improved engine power and efficiency, reduced "turbo" lag, high reliability combined with compact size of components and robust construction. The arrangement is not expensive to manufacture

and can be linked in to the engine management system. It may also provide an opportunity for the vehicle alternator to be removed for being redundant.

Many further modifications and variations will suggest themselves to those versed in the art upon making reference to the foregoing description which is given by way of example only and is not intended to limit the scope of the invention, that being determined by the appended claims.

CLAIMS

1. A motor comprising two or more rotors rotated by means of a common power supply, each rotor having a plurality of poles and being associated with a stator having a plurality of poles, wherein the arrangement of rotor poles and stator poles is different for each rotor so that the rotors rotate at different speeds when the common power supply is applied.
2. A motor as claimed in claim 1, wherein the number of stator poles is the same for each rotor, but the number of rotor poles is different.
3. A motor as claimed in claim 2, wherein a common stator is provided for the rotors.
4. A motor as claimed in claim 1 or 2, wherein separate stators are provided for each rotor and the windings on each stator are electrically connected.
5. A motor as claimed in claim 4, wherein switches are provided for breaking the interconnection between the windings on different stators in order to independently stop the rotation of one or more of the rotors.
6. A motor as claimed in claim 4 or 5, wherein the interconnection between the windings can be intermittently interrupted in order to facilitate starting and/or stopping of one or more of the rotors.
7. A motor as claimed in any one of claims 4 to 6, wherein means are provided for varying the ratio of speeds between the rotors in discrete steps by sequencing the pattern of electrical interconnections between the windings.
8. A motor as claimed in any one of the preceding claims, wherein means are provided for causing at least one of the rotors to rotate in a direction opposite to the direction of rotation of the remaining motor or motors.

9. A motor as claimed in claim 8, wherein the said means comprise magnets which are located in such positions as to prime the rotors, when stationary, for rotation in mutually opposite directions by locating each rotor pole closer to a predetermined one of two adjacent stator poles.
10. A motor as claimed in any one of the preceding claims, wherein a first rotor and a second rotor each operate as a switched reluctance motor.
11. A motor as claimed in any one of claims 1 to 9, wherein a first rotor and a second rotor each operate as a stepper motor.
12. A motor as claimed in any one of claims 1 to 9, wherein a first rotor operates as a switched reluctance motor and a second rotor operates as a stepper motor.
13. A motor as claimed in any one of the preceding claims, wherein the motor is adapted for use in a vacuum cleaner.
14. A motor as claimed in claim 13, wherein one of the rotors is adapted to drive the impeller of the vacuum cleaner.
15. A motor as claimed in claim 14, wherein a second of the rotors is adapted to drive a second impeller of the vacuum cleaner.
16. A motor as claimed in any one of claims 13 to 15, wherein one of the rotors is adapted to drive a brush bar of the vacuum cleaner.
17. A motor as claimed in any one of claims 1 to 12, wherein the second rotor forms part of a switched reluctance generator.

18. A motor as claimed in claim 17, wherein the first rotor is used to drive the compressor of a turbo charger and the switched reluctance generator is adapted to absorb the energy of the turbine.
19. A motor substantially as hereinbefore described with reference to any one of the embodiments shown in the accompanying drawings.
20. A vacuum cleaner incorporating a motor as claimed in any one of the preceding claims.

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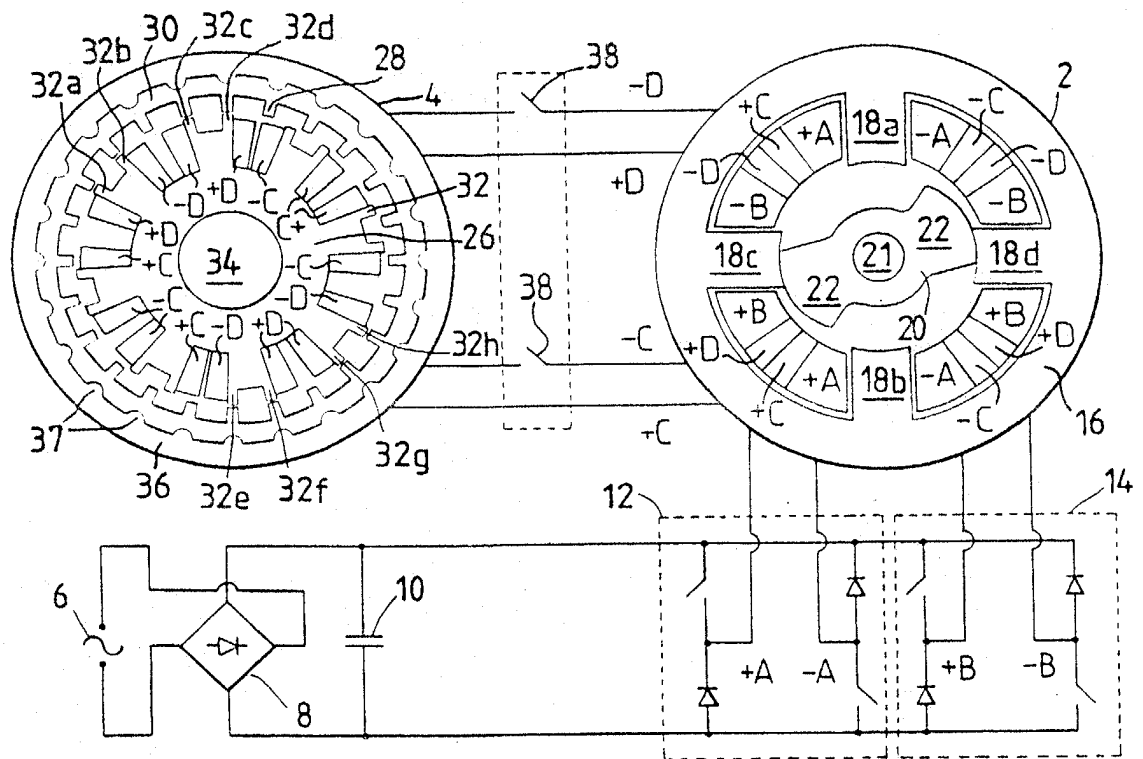


FIG.1

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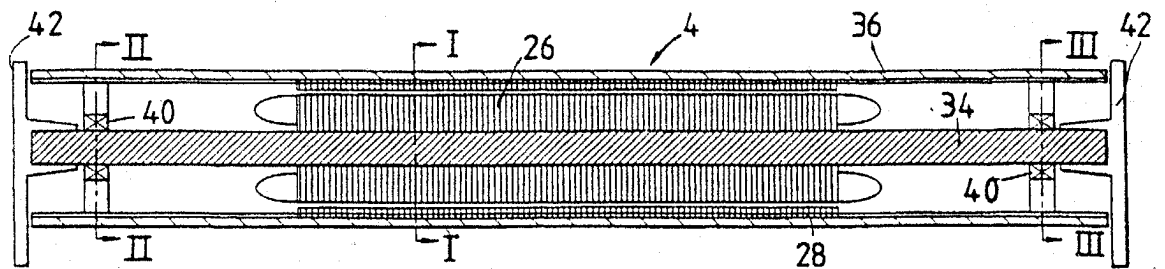


FIG. 2a

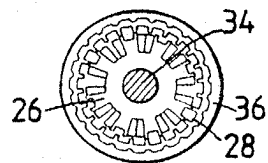


FIG. 2b

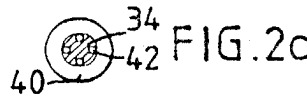


FIG. 2c

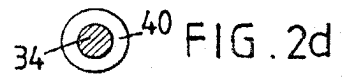


FIG. 2d

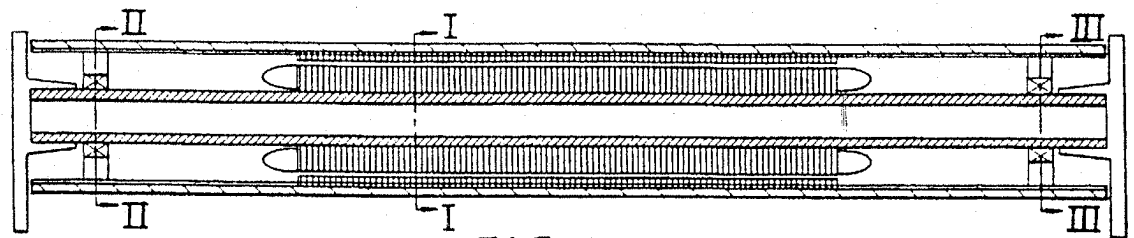


FIG. 3a

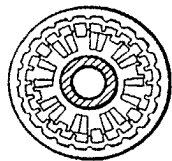


FIG. 3b

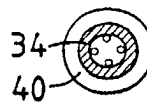


FIG. 3c

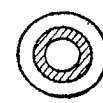


FIG. 3d

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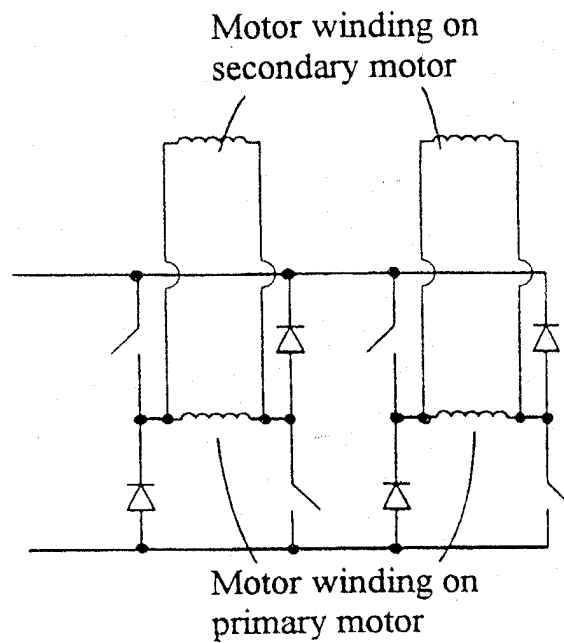


FIG. 4a

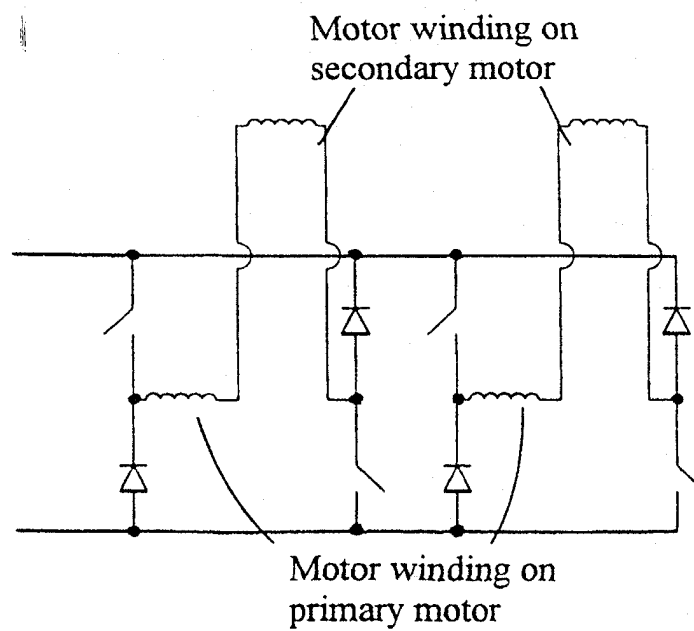


FIG. 4b

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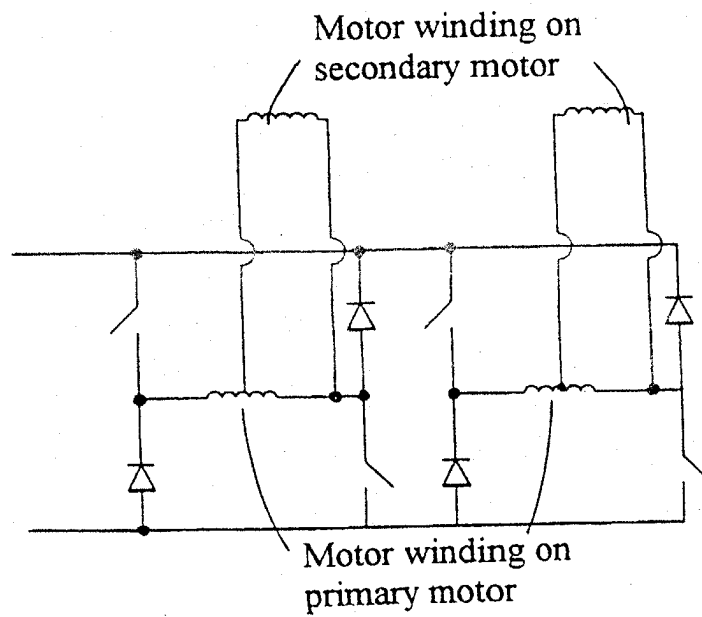


FIG. 4c

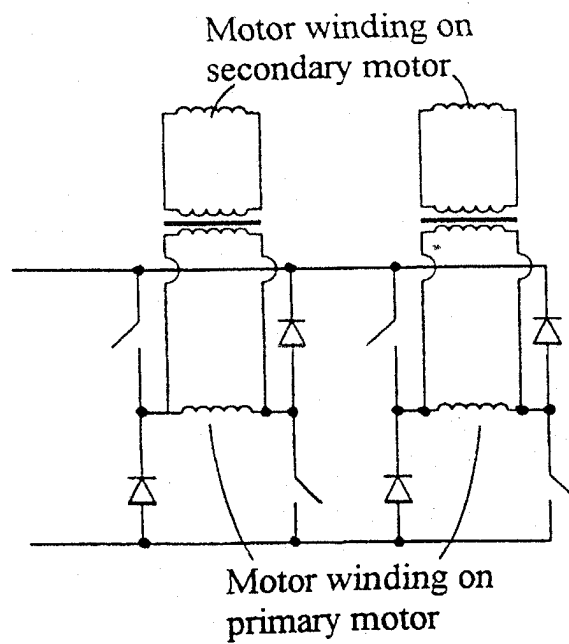


FIG. 4d

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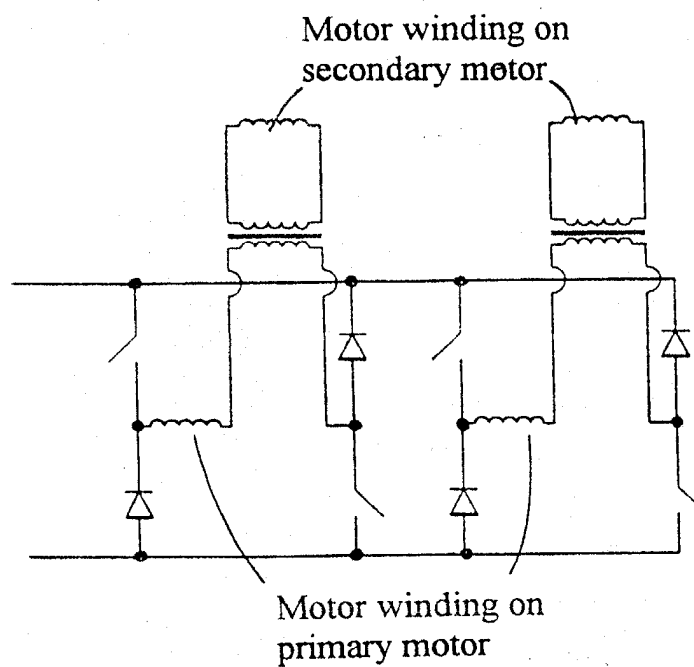


FIG. 4e

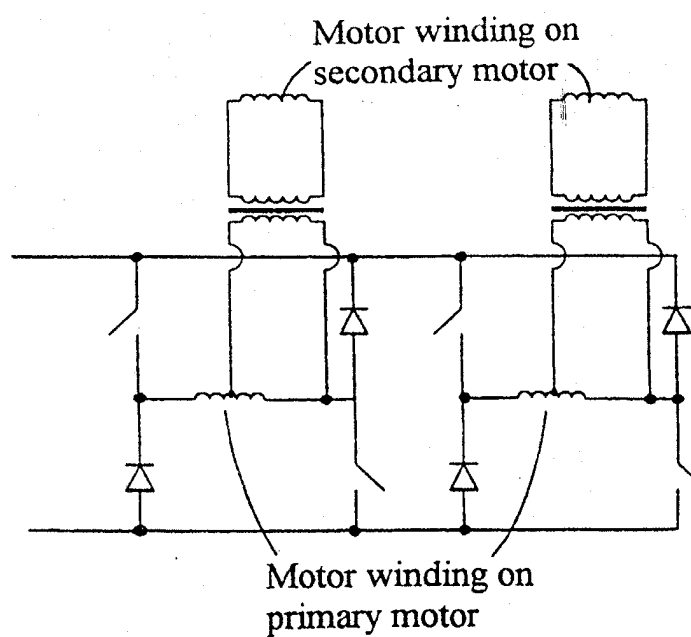


FIG. 4f

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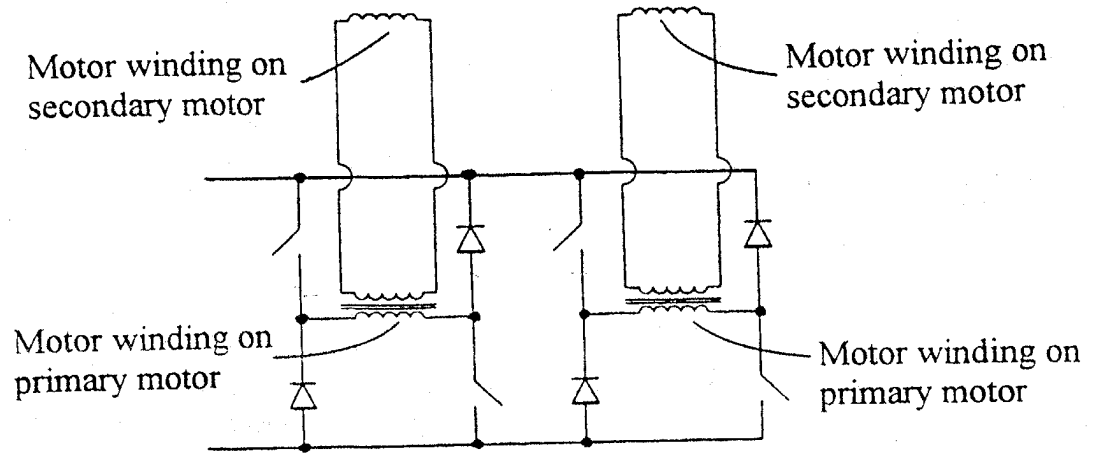


FIG. 4g

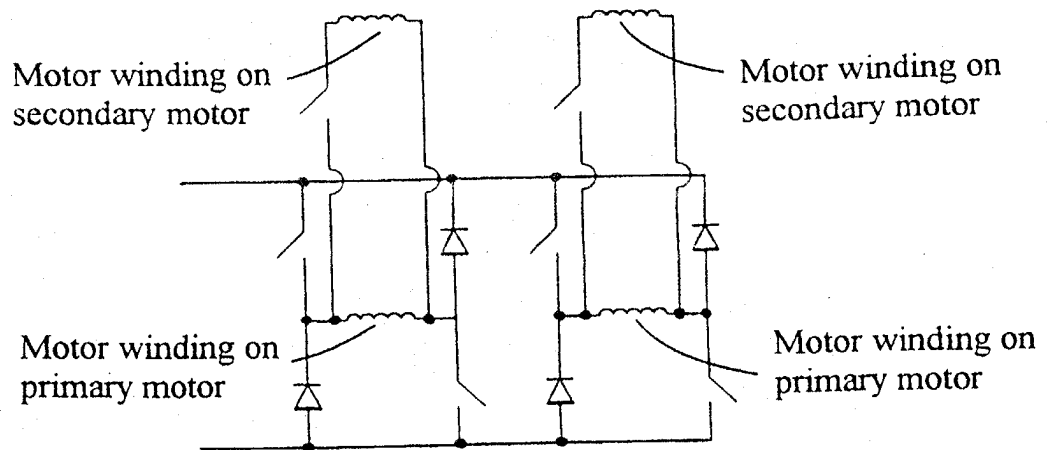


FIG. 4h

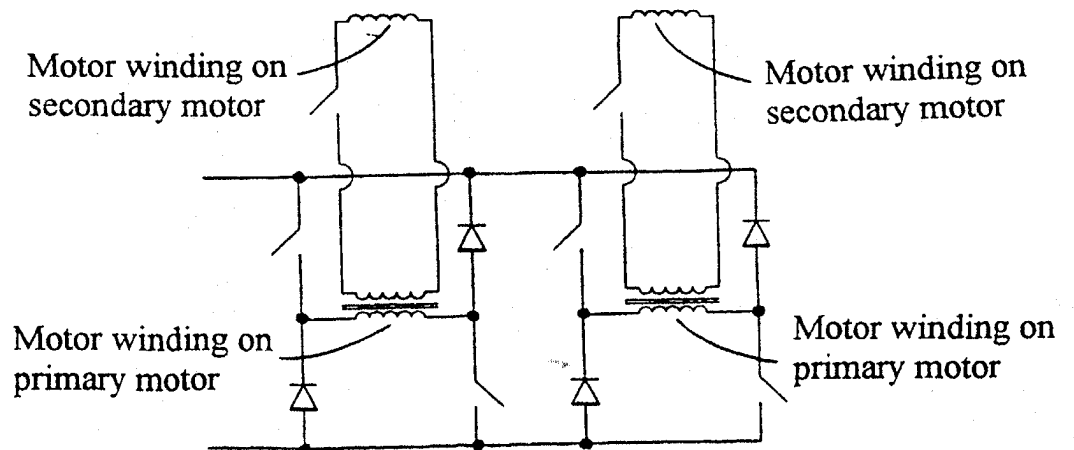


FIG. 4i

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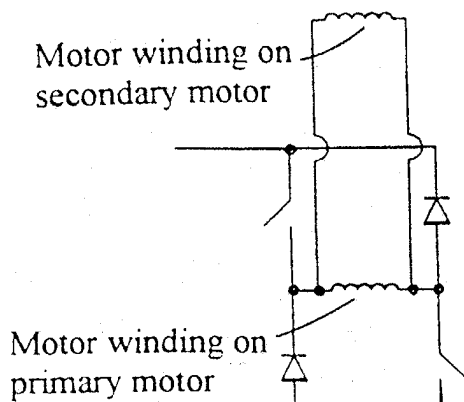


FIG. 5a

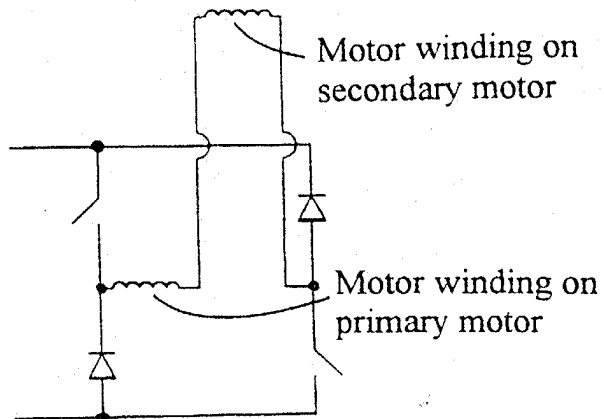


FIG. 5b

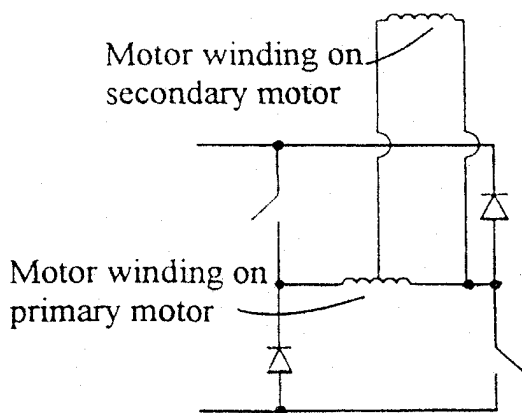


FIG. 5c

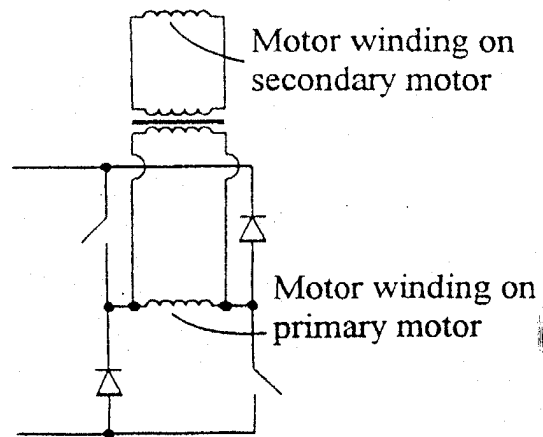


FIG. 5d

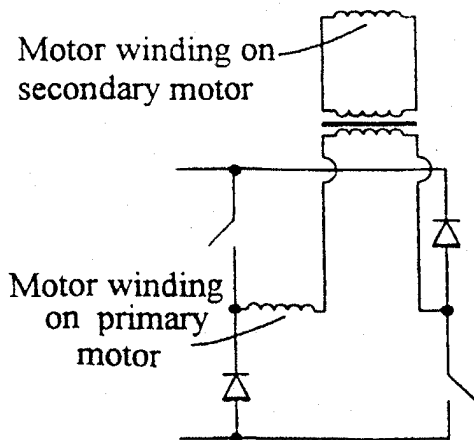


FIG. 5e

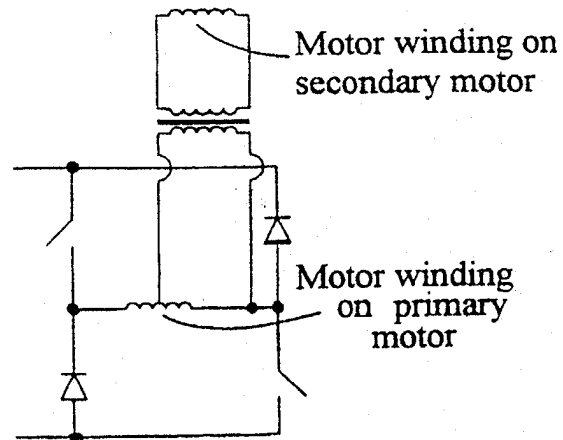


FIG. 5f

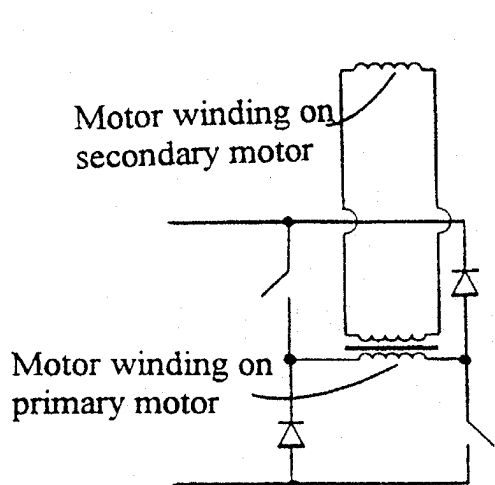


FIG. 5g

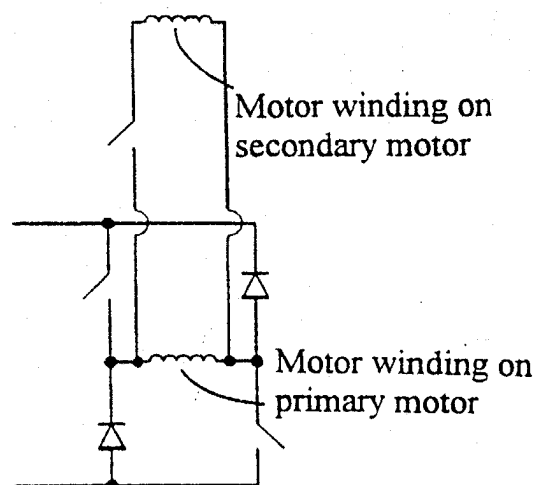


FIG. 5h

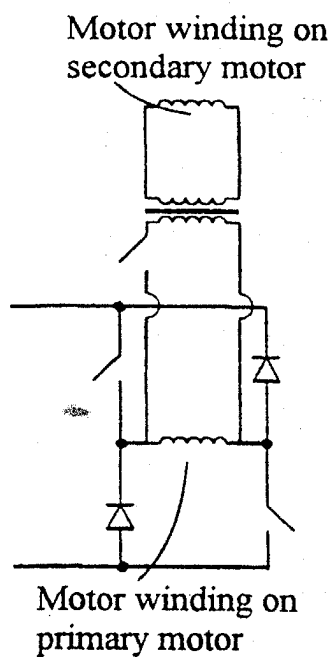


FIG. 5i

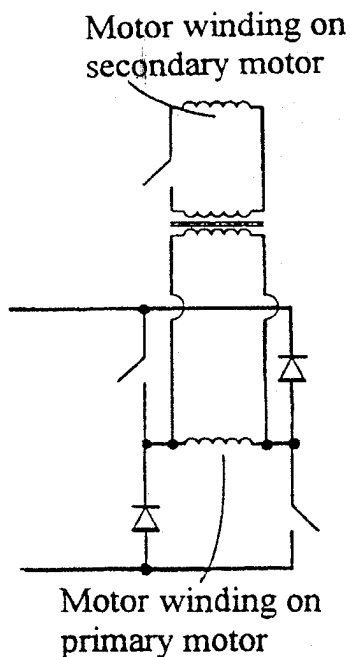


FIG. 5j

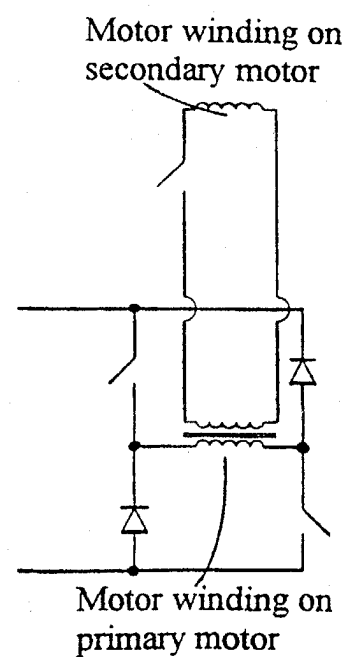


FIG. 5k

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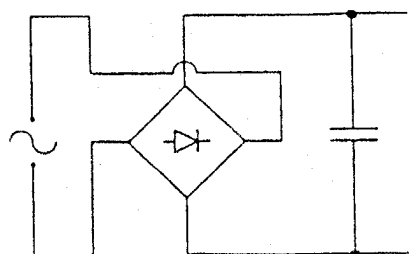


FIG. 6a

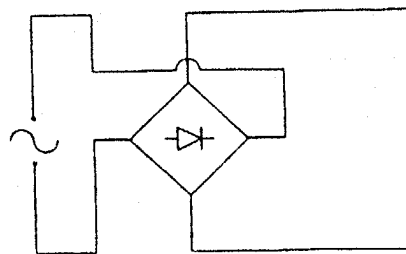


FIG. 6b

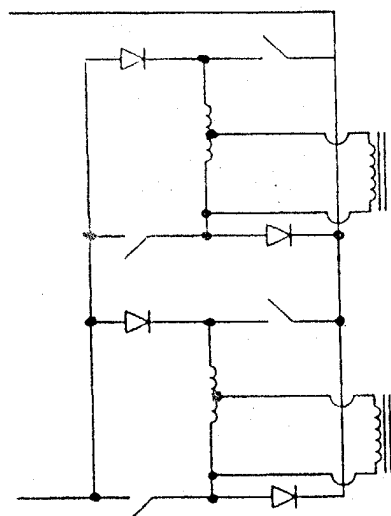


FIG. 6c

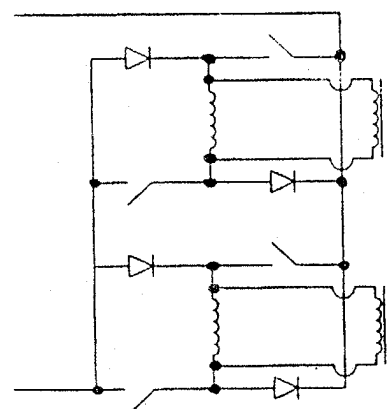


FIG. 6d

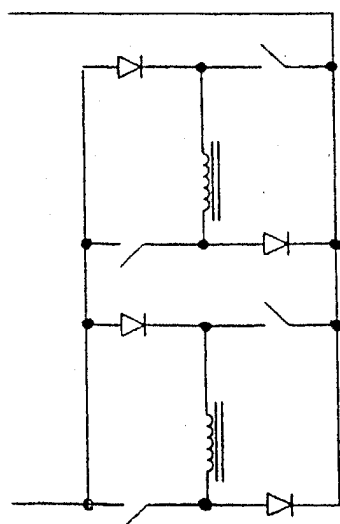


FIG. 6e

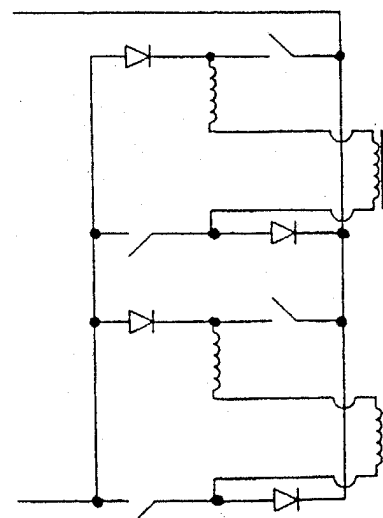


FIG. 6f

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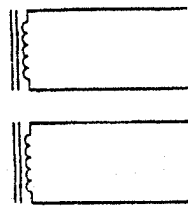


FIG. 6g

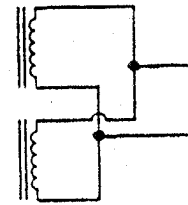


FIG. 6h

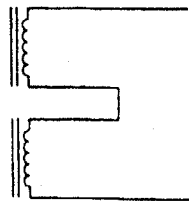


FIG. 6i

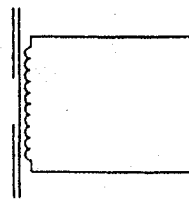


FIG. 6j



FIG. 6k

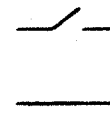


FIG. 6l

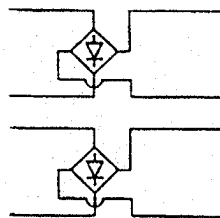


FIG. 6m

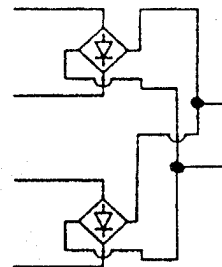


FIG. 6n

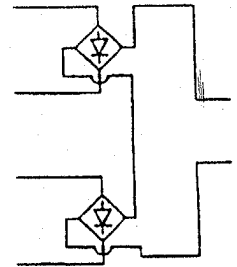


FIG. 6o

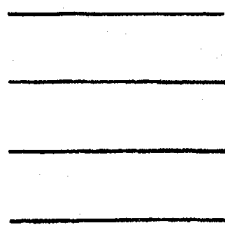


FIG. 6p

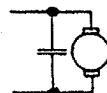


FIG. 6q

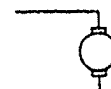


FIG. 6r

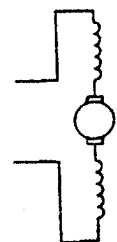


FIG. 6s

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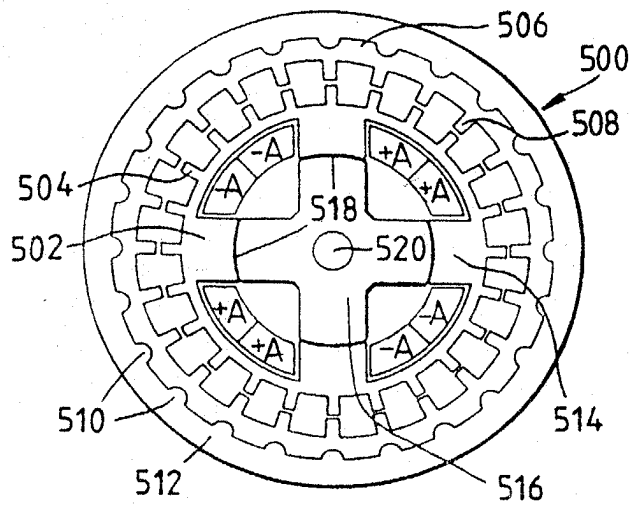


FIG. 7a

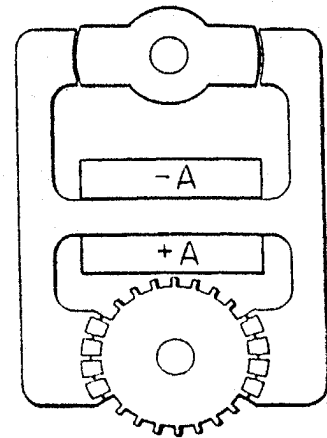


FIG. 7b

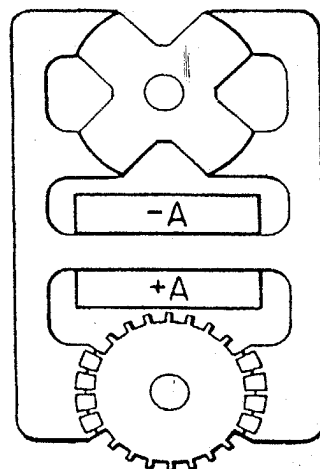


FIG. 7c

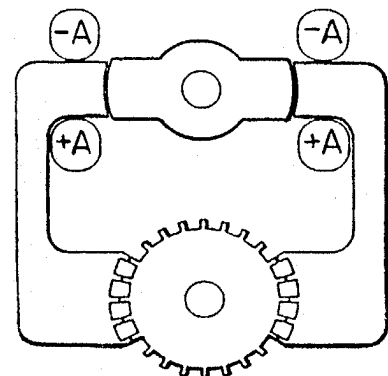


FIG. 7d

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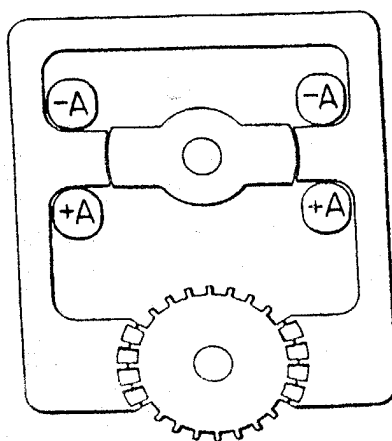


FIG. 7e

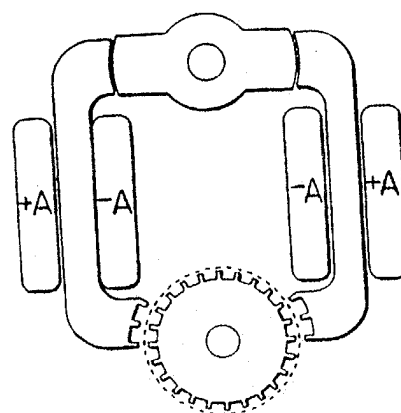


FIG. 7f

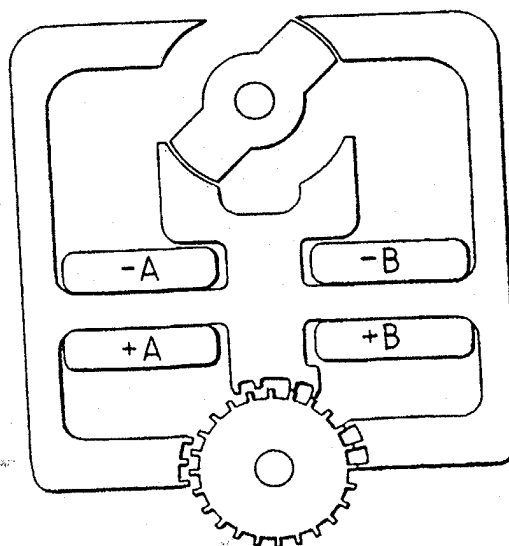


FIG. 7g

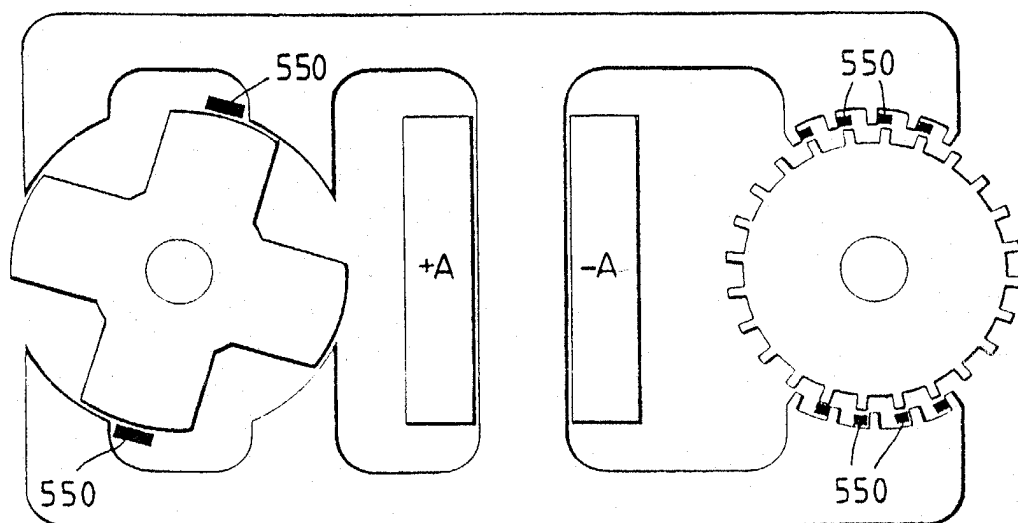


FIG. 8a

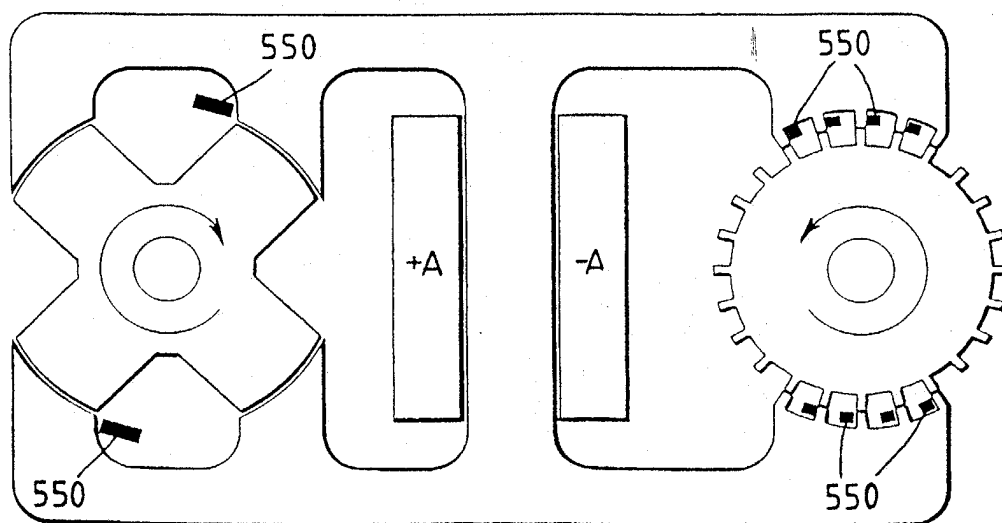
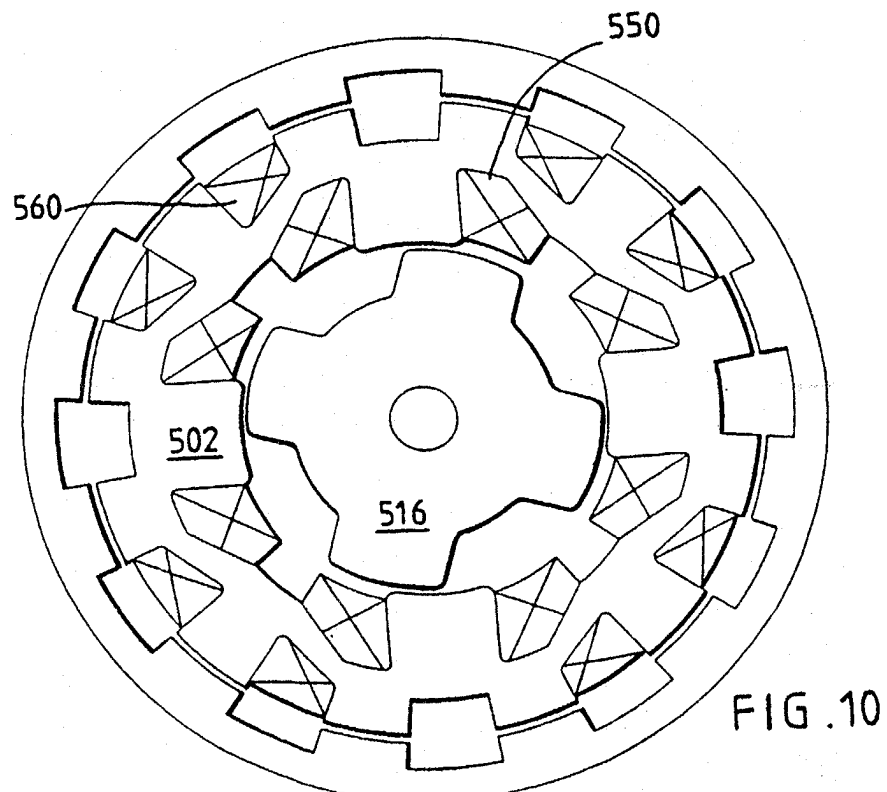
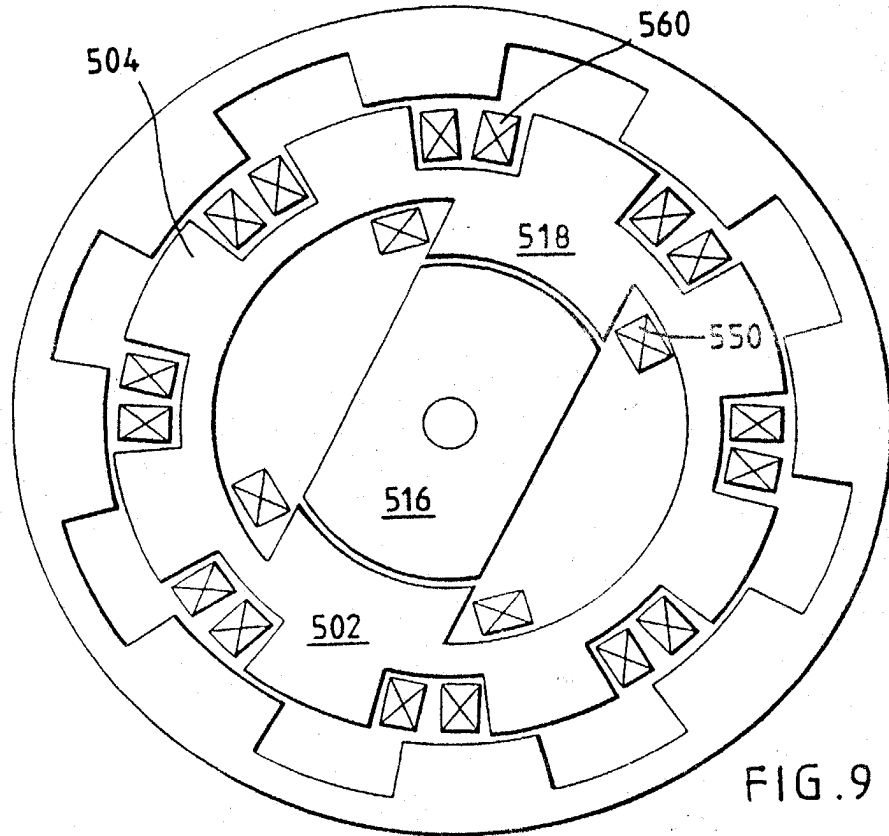


FIG. 8b

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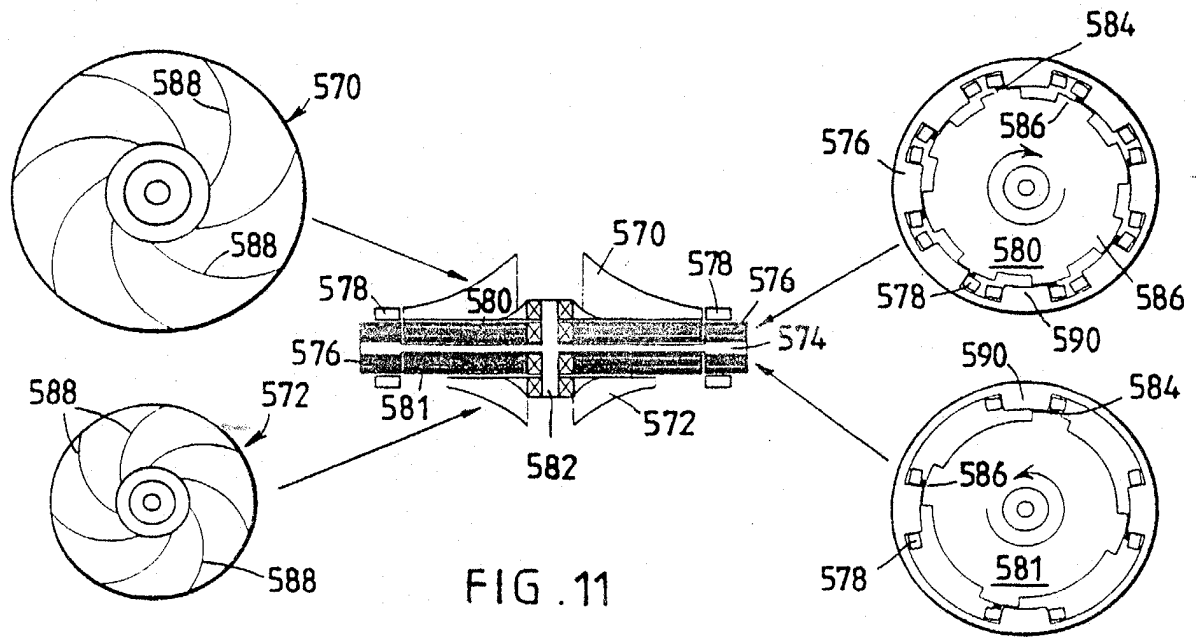


FIG. 11

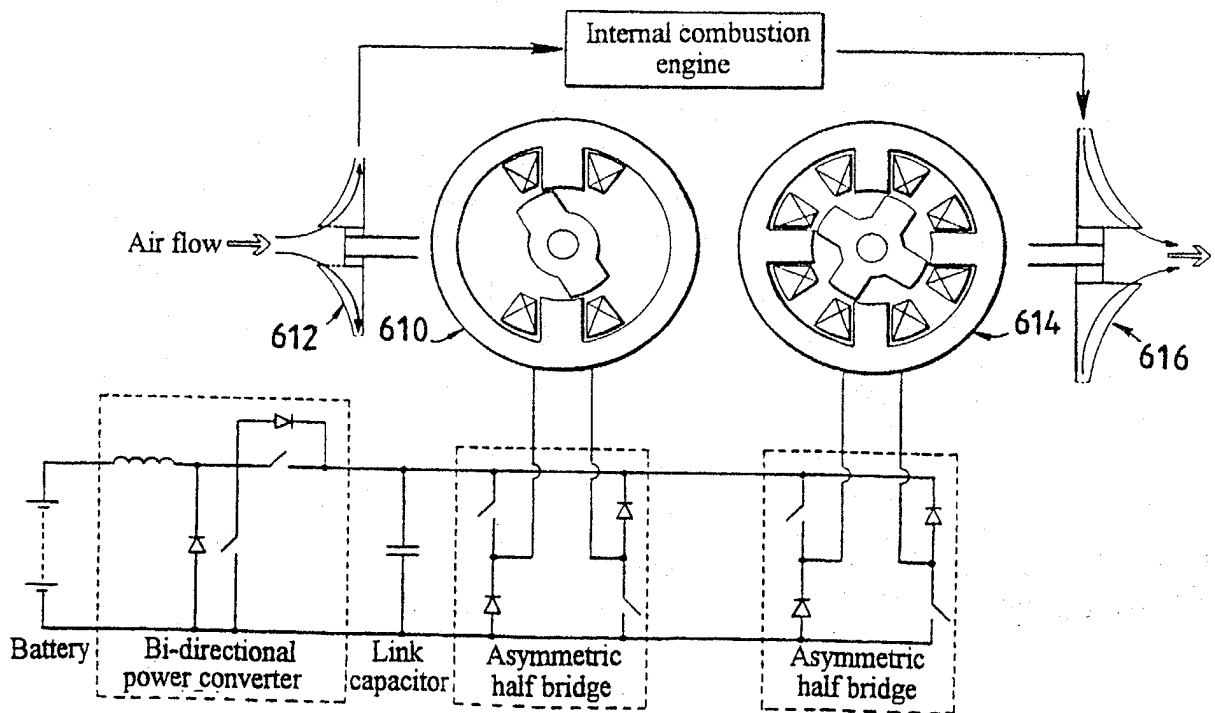


FIG. 12

INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 98/01304

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 H02K16/02 H02P7/74

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 H02K H02P

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	GB 2 255 859 A (MULFINGEN ELEKTROBAU EBM) 18 November 1992 see page 2, line 7 - page 2, line 19 see page 6, line 13 - page 6, line 16	1-20
Y	US 4 164 852 A (ANZALONE CARMEN J) 21 August 1979 see figure 1	1-4
Y	GB 1 198 526 A (LICENTIA GMBH) 15 July 1970 see page 1, right-hand column, line 70 - page 1, right-hand column, line 75 see page 3, left-hand column, line 7 - page 3, left-hand column, line 13 -/-	5-7

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

18 August 1998

Date of mailing of the international search report

25/08/1998

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INTERNATIONAL SEARCH REPORT

Int. onal Application No

PCT/GB 98/01304

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5 124 606 A (EISENBEIS GOTTFRIED) 23 June 1992 see column 3, line 21 - column 3, line 47 ---	8,9
Y	GB 2 227 127 A (SUNDSTRAND CORP) 18 July 1990 see figures 1,9 ---	10-12
Y	US 4 225 999 A (MARTINEC EUGENE F ET AL) 7 October 1980 see abstract ---	13-15,20
Y	PATENT ABSTRACTS OF JAPAN vol. 014, no. 134 (C-0701), 14 March 1990 & JP 02 007923 A (MATSUSHITA ELECTRIC IND CO LTD), 11 January 1990 see abstract ---	16
Y	US 4 745 754 A (KAWAMURA HIDEO) 24 May 1988 see figure 1 ---	17,18
Y	EP 0 746 084 A (EBAUCHESFABRIK ETA AG) 4 December 1996 see abstract; figures 1-3 ---	19
A	DE 33 13 768 A (ELEKTROMOTOREN SAVOD ELPROM) 18 October 1984 see abstract; figure 1 -----	1

INTERNATIONAL SEARCH REPORT

Information on patent family members

Inter. onal Application No

PCT/GB 98/01304

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